

## METHOD OF ENHANCING THE EXTRACTION OF PROTEINASE INHIBITORS

### Background of the Invention

#### 1. Field of the Invention

5 The present invention relates to a method of enhancing the extraction of a proteinase inhibitor, and more specifically, to a method of improving the yield and purity of Proteinase Inhibitor-II (PI<sub>2</sub>) extracted from whole potatoes.

#### 2. Background of the Prior Art

10 The extraction, isolation and purification of plant-derived proteins is well known in the field of biochemistry. In 1972, Melville and Ryan reported a large-scale preparation for isolating Chymotrypsin Inhibitor I from potato tubers (Melville, J.C. and Ryan, C.A. Chymotrypsin inhibitor I from potatoes. J. Biological Chem., 247: 3445-3453, 1972). According to the method of Melville and Ryan, potatoes were sliced with peels intact and soaked in a sodium dithionite solution, homogenized, and expressed through nylon cloth. The resulting juice was adjusted to pH 3, centrifuged at 1000 x g for 15 minutes at 5° F, and the supernatant collected and fractionated with ammonium sulfate.

15 Purification was achieved through water washing and heat treatment whereby clear filtrates of heated fractions were pooled and lyophilized. Suspending the lyophilized powder in water, dialyzing it against water for 48 hours, and lyophilizing the resulting clear filtrate obtained a crude extract. Resuspended extract was then centrifuged and applied to a column of Sephadex G-75. Collected fractions containing the Inhibitor I were pooled, evaporated, and desalted on a column of Sephadex G-25. The resulting gel-filtered inhibitor product was determined to be approximately 90% Inhibitor I protein purified by dissociation on a Sephadex G-75 column and desalted on a column of Sephadex G-25.

20 The Ryan lab followed-up by reporting the isolation and characterization of Proteinase Inhibitor II in much the same manner as described for Inhibitor I (Bryant, J., Green, T.R., Gurusaddaiah, T., Ryan, C.L. Proteinase inhibitor II from potatoes: Isolation and characterization of its protomer components. Biochemistry 15: 3418-3424, 1976). Bryant et al. differentiated potato-derived proteinase inhibitors into two groups based on their respective stabilities to a temperature of 80° C for 10 minutes. Proteinase Inhibitor I (PI<sub>1</sub>) is characterized as a tetrameric

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protein composed of four hybridized isoinhibitor protomer species having a molecular weight of 39,000, whereas PI<sub>2</sub> is characterized as a dimeric inhibitor comprising four isoinhibitor promoter species having a molecular weight of 21,000.

The extraction and isolation of proteinase inhibitor proteins from potatoes is described in WO 99/01474. Proteins from potato tubers are extracted in soluble form in an aqueous/alcohol extraction medium, such as dilute formic acid and 20% ethanol. The alcohol extract is heated to a first temperature to denature most of the unwanted proteins and cooled to a second temperature to form a precipitate phase constituting the debris and a soluble phase that contains the heat stable proteinase inhibitor proteins. The heat stable proteinase inhibitor proteins are precipitated from the soluble phase by dialysis against a suitable dialysis medium, such as dilute formic acid.

Recently, PI<sub>2</sub> has been implicated in playing a role in extending satiety in subjects fed a nutritional drink composition containing PI<sub>2</sub>. U.S. Patent Application Serial No. 09/624,922 describes that subjects reported a significant reduction in hunger for up to 3 ½ hours post meal when fed a meal comprising a nutritional drink composition containing PI<sub>2</sub>. Likewise, fullness ratings were enhanced, and each study subject lost an average of 2 kg over a 30-day period without experiencing the adverse side effects typically associated with appetite suppressing compounds. Mechanistically, it is thought that as a trypsin and chymotrypsin inhibitor, when consumed by a subject, PI<sub>2</sub> stimulates the release of endogenous cholecystokinin, a known putative feedback agent effective in reducing the desire to intake food.

Existing methods for the extraction of proteinase inhibitors involve several laborious and time consuming steps and result in losses of yield and reduced purity of the recovered proteinase inhibitor. In addition, the most promising prior art methods rely on the use of ethanol in the extractant solution which, at the concentrations used, makes the solution flammable. None of the prior art processes have been demonstrated on a commercial scale. Accordingly, a need exists for a large-scale extraction process to extract PI<sub>2</sub> in a cost-effective and efficient manner meeting industrial qualitative and quantitative standards.

### Summary of the Invention

Plant material containing a desired proteinase inhibitor is combined with a solution of an organic acid and a salt. The plant material is comminuted, forming a slurry in the acid and salt

solution, to reduce the particle size and increase the surface area of the particles to improve the efficiency of the extraction. The process of comminution is selected to reduce the particle size without denaturing the desired proteinase inhibitor through local heating effects. The acid and salt solution enhances the extraction of the proteinase inhibitor from the comminuted plant material and protects it against degradation by other compounds that may be released from the ruptured plant cells. Once extracted into solution, the proteinase inhibitor is isolated and purified by centrifugation, clarification, filtration and drying of the extract solution. The acid and salt are removed during the filtration stage so as not to adulterate the purified proteinase inhibitor product.

In a preferred embodiment, proteinase inhibitor II (PI2) is extracted from whole potato tubers. Organic acids known to be effective in the process include acetic, ascorbic, citric and formic acid. Formic acid was found to result in the highest purity and highest yield of the final PI2 product. The formic acid content of the solution is adjusted in the range of 0.5% to 2.5% w/w, with a preferred content of approximately 1.5%. Sodium chloride is added to the extractant solution to increase the solubility of the potato proteins. Sodium chloride concentrations of between 1 N and 3 N are used, with a preferred concentration of approximately 1.5 N. The solution is added to the potatoes in a weight ratio of between 1:1 and 1:10, with a preferred ratio of 1:2.5 extraction solution:potato, w/w, respectively.

Comminution is accomplished by grinding. A target particle size is in the range of 100 to 1500  $\mu\text{m}$ . In this range, product yields were increased and flow characteristics of the slurry were acceptable. Decreasing the particle size below 100  $\mu\text{m}$  resulted in a lower recovery of PI2 and did not improve the flow characteristics. Grinding for an extended period of time also resulted in a reduced PI2 yield, most likely due to an increase in temperature and the release of undesired proteases that reduce the PI2 yield. The formic acid and sodium chloride are efficiently removed during the filtration stage.

An object of the present invention is to provide an improved method for the extraction of proteinase inhibitors from plant materials.

Another object of the invention is to provide an improved method for the extraction of proteinase inhibitor II from potato tubers which does not rely on the use of ethanol in the extraction solution.

A further object of the invention is to provide a method of extracting proteinase inhibitor II from potato tubers that is efficient and cost-effective on a commercial scale.

#### Detailed Description of the Invention

5           The extraction and isolation of PI2 from potatoes begins with the addition of an organic acid, preferably formic acid, and a salt, preferably sodium chloride, to raw potatoes. The mixture is subjected to comminution to reduce the particle size of the potato particles and extract soluble proteins. Centrifugation is used to remove solids and the liquid fraction is heated at a temperature sufficient to denature many undesired proteins but not PI2. The solution is again  
10       centrifuged to remove the insoluble denatured proteins and the liquid fraction is microfiltered to remove relatively large particles. Ultrafiltration is used to remove the organic acid and salt and further purify the PI2 in the retentate.

          A process for the extraction of PI2 from whole potatoes was developed in an attempt to maximize yield, minimize impurities, minimize cost, and achieve commercial feasibility. The extraction solution was evaluated based on the ability of the process to solubilize the PI2, protect the PI2 from degradation, and maximize total PI2 removed from the insoluble potato components, while minimizing the amount of co-solubilized proteins. The extraction solution incorporated the solubility and functional stability of PI2 in acidic media and at elevated temperatures. An extraction solution containing sodium chloride and formic acid has been found  
20       effective for this purpose. The ratio of extraction solution utilized to raw material extracted was minimized for cost purposes, while producing the maximum yield of PI2 per kilogram of raw potato tubers.

#### Reverse Phase HPLC Method

25           The amount of PI2, Kunitz and carboxypeptidase inhibitors was measured using reverse phase HPLC. A Microsorb C-18 column (4.6 mm x 250 mm, 5  $\mu$ m particles with 300 Angstrom pore size; Varian Analytical Instruments) was used. Two mobile phase solvents were prepared, solvent A was 800 g deionized H<sub>2</sub>O, 150 g acetonitrile, and 0.95 trifluoroacetic acid, and solvent B was 850 g acetonitrile and 0.85 g trifluoroacetic acid. Approximately 50 mg of the sample  
30       was added to 100 ml of solvent A. The sample was vortexed for 30 seconds, and then

centrifuged at 10,000 rpm for 10 minutes. The supernatant was collected for RP-HPLC analysis. One hundred  $\mu$ l of the sample was injected into the column, with the pump set at 800 - 2500 psig, and a temperature of 30.0° C. The other flow rate, time, and solvent compositions are as set out in Table 1. The diode array of the detector was set at 220 nm.

Table 1. HPLC Conditions

Time (min)	Flow rate (ml/min)	Solvent Composition (volume %)
0	1	100 %A
5	1	100%A
34	1	38% A
38	1	100% B
40	2	100%B
45	2	100%B
50	1	100%A
55	1	100%A

An external standard was prepared to construct a standard curve for calibration of the column. Five mg of BSA were dissolved in 10 ml of solvent A. Four volumes, i.e., 25, 50, 75, and 100  $\mu$ l, were injected into the column. A calibration curve was generated from the results.

#### Example 1

Five hundred grams of potato tubers were extracted with 213 ml of 1% formic acid solution in a Waring blender for 2.5 minutes. The slurry was centrifuged at 10,000 rpm for 40 minutes. The liquid was decanted and filtered through #4 Whatman filter paper, yielding 486 g of clarified extract. Fifty grams of this clarified extract was poured into each of six 125 ml Erlenmeyer flasks equipped with magnetic stir bars. The amount of NaCl corresponding to Table 2 was added to each flask and stirred until the salt was dissolved. The flasks were then heated on high with stirring on a hot plate until the temperature of the extract reached 70° C. After ambient cooling to room temperature, the solutions were centrifuged at 12,000 rpm for 5 minutes and then analyzed using the above-described reverse phase HPLC method. The reported level of PI2 was calculated by integrating the area of the PI2 peak. The injection volume was 100  $\mu$ l and the following equation was used to equate peak areas to protein levels:

$$\text{Protein (mg/ml)} = \left[ \left( \frac{\text{peak area}}{4} \right) \times 8.17 \times 10^{-5} \right] + 0.0338$$

To clarified potato extract was added varying amounts of sodium chloride, followed by heating to 70° C for 10 minutes. After cooling to room temperature, the solutions were analyzed for the protein eluting after PI2 in the HPLC method for PI2 quantification. The results are shown in Table 2.

Table 2 - Protein Removal with Varying Sodium Chloride Levels

[NaCl] N	Protein Eluting at 16-30 minutes mg/ml	Protein Eluting at ~23-30 minutes mg/ml	PI2 Level mg/ml
0.0	0.504	0.378	0.167
0.1	0.298	0.184	0.160
0.2	0.245	0.141	0.172
0.3	0.178	0.076	0.149
0.4	0.150	0.071	0.169
0.5	0.119	0.076	0.189

To establish the removal of Kunitz impurities from the potato extract, which have been shown to diminish the effectiveness of PI2 to increase satiety, the reverse phase HPLC method was used on a commercially available Kunitz standard purchased from SIGMA. A chromatograph of the Kunitz standard revealed that the major peak of the Kunitz impurities appears at approximately 25 minutes. Another inhibitor known to be present in potatoes is the carboxypeptidase inhibitor. The reverse phase HPLC method was used on a commercially available carboxypeptidase standard purchased from SIGMA. A chromatograph of the carboxypeptidase standard revealed that the major peaks of the carboxypeptidase impurities is a doublet that appears at approximately 17 minutes. At a level of 0.3 N sodium chloride and above, the post heat-treatment protein level remains relatively constant. The amount of PI2 remained relatively constant for all trials, indicating that at 70° C no PI2 is precipitated at the salt levels up to 0.5 N. In order to reach the level of NaCl required in the heat-treatment phase, it is necessary to use an extractant with approximately 2 times the desired final salt concentration. Accordingly, a salt level of at least 0.3 N is desirable in the extraction solution during heat treatment at 70° C to

ensure efficient removal of Kunitz type proteins. Purity of the final PI2 product can be improved with greater amounts of sodium chloride.

## Example 2

An optimization study was performed to determine both the proper NaCl content and formic acid content of the extraction solution. The ideal extraction solution formulation would maximize the amount of PI2 liberated from the potato matrix, while minimizing the amount of protein contaminants solubilized. The liberation of PI2 was measured as yield, normalized to an extraction solution composition of 1.0 N NaCl. This was chosen as the normalization basis due to the previously stated prediction necessitating a two-fold increase of NaCl beyond the 0.5 N system shown effective for impurity removal in the heat-treatment stage. For optimization purposes, PI2 protein purity was measured and compared empirically to the normalized extraction yields. Extraction solutions containing NaCl concentrations from 0.0 N to 2.0 N were examined. In a similar manner, the formic acid content of the extraction solution was optimized. Formic acid contents ranging from 0.0 percent to 2.5 percent were studied.

Table 3 - Sodium Chloride Optimization Data

[NaCl] N	PI2 Area	Doublet Area	Time (min)	"Kunitz" Area	Time (min)
0.0	4283.0	6402.2	17.28	83436.8	~23.5 - 29.0
1.0	6627.8	6294.6	17.28	131502.6	~23.5 - 29.0
1.0	4771.1	5571.2	16.97	113666.7	~23.5 - 29.0
2.0	5146.2	5306.3	16.95	120910.1	~23.5 - 29.0
0.0	4712.8	6231.8	17.48	83908.4	~23.5 - 29.0
0.5	6592.7	6932.0	17.48	125256.4	~23.5 - 29.0
1.0	7578.4	7425.0	17.47	128660.5	~23.5 - 29.0
2.0	6822.6	6890.4	17.46	130632.2	~23.5 - 29.0
0.0	4235.2	6130.1	17.74	90357.4	~24.0 - 29.5
0.7	5964.6	6606.2	17.72	135932.2	~24.0 - 29.5
1.0	6746.7	6531.5	17.50	126617.3	~23.5 - 29.0
1.3	6062.5	6163.9	17.69	142488.8	~24.0 - 29.5
0.0	4699.6	6065.3	17.54	89125.2	~23.75 - 29.25
1.0	7768.5	6008.5	17.54	138907.2	~23.75 - 29.25
1.3	8095.2	6513.1	17.54	151858.8	~23.75 - 29.25
0.0	4743.7	5563.6	17.70	80937.5	~24.0 - 29.5
0.5	5825.3	5577.7	17.69	120352.4	~24.0 - 29.5
1.0	6848.1	5260.6	17.75	129407.5	~24.0 - 29.5

1.3	7173.2	5365.8	17.53	142758.6	~24.0 - 29.5
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Table 4 - Sodium Chloride Optimization Data Continued

[NaCl] N	PI2 Area	PI2 (mg/ml)	Doublet Area	Protein (mg/ml)	"Kunitz" Area	Protein (mg/ml)
0.0	4283.0	0.16	6402.2	0.20	83436.8	1.73
1.0	6627.8	0.21	6294.6	0.20	131502.6	2.68
1.0	4771.1	0.17	5571.2	0.19	113666.7	2.32
2.0	5146.2	0.18	5306.3	0.18	120910.1	2.47
0.0	4712.8	0.17	6231.8	0.20	83908.4	1.73
0.5	6592.7	0.21	6932.0	0.21	125256.4	2.55
1.0	7578.4	0.23	7425.0	0.22	128660.5	2.62
2.0	6822.6	0.21	6890.4	0.21	130632.2	2.66
0.0	4235.2	0.16	6130.1	0.20	90357.4	1.86
0.7	5964.6	0.19	6606.2	0.21	135932.2	2.76
1.0	6746.7	0.21	6531.5	0.20	126617.3	2.58
1.3	6062.5	0.20	6163.9	0.20	142488.8	2.89
0.0	4699.6	0.17	6065.3	0.20	89125.2	1.84
1.0	7768.5	0.23	6008.5	0.19	138907.2	2.82
1.3	8095.2	0.24	6513.1	0.20	151858.8	3.08
0.0	4743.7	0.17	5563.6	0.19	80937.5	1.68
0.5	5825.3	0.19	5577.7	0.19	120352.4	2.46
1.0	6848.1	0.21	5260.6	0.18	129407.5	2.63
1.3	7173.2	0.22	5365.8	0.18	142758.6	2.90

TABLE 4 - Sodium Chloride Optimization Data Continued



Table 5 - Sodium Chloride Optimization Data Continued

[NaCl] N	PI2 (mg/ml)	PI2 mg	Normalized yield	Doublet (mg/ml)	Doublet (mg)	Kunitz (mg/ml)	Total Kunitz (mg)	Purity
0.0	0.16	78.25	77.51%	0.20	98.76	1.73	844.50	7.66%
1.0	0.21	100.75	100.00%	0.20	97.53	2.68	1307.21	6.69%
1.0	0.17	79.59	100.00%	0.19	87.02	2.32	1090.74	6.33%
2.0	0.18	82.23	104.38%	0.18	83.70	2.47	1146.21	6.27%
0.0	0.17	81.88	74.82%	0.20	96.49	1.73	843.57	8.01%
0.5	0.21	100.78	91.34%	0.21	104.07	2.55	1251.43	6.92%
1.0	0.23	104.63	100.00%	0.22	103.22	2.62	1218.05	7.34%
2.0	0.21	97.11	93.36%	0.21	97.73	2.66	1228.97	6.82%
0.0	0.16	72.99	82.29%	0.20	90.21	1.86	855.33	7.17%
0.7	0.19	88.27	92.58%	0.21	94.07	2.76	1263.08	6.11%
1.0	0.21	100.78	100.00%	0.20	98.72	2.58	1246.21	6.97%
1.3	0.20	93.49	93.51%	0.20	94.45	2.89	1386.67	5.94%
0.0	0.17	80.77	73.47%	0.20	93.75	1.84	883.03	7.64%
1.0	0.23	111.08	100.00%	0.19	94.18	2.82	1370.31	7.05%
1.3	0.24	113.59	102.82%	0.20	98.48	3.08	1486.42	6.69%
0.0	0.17	80.41	80.24%	0.19	88.13	1.68	797.53	8.32%
0.5	0.19	92.04	90.39%	0.19	89.68	2.46	1187.23	6.72%
1.0	0.21	100.96	100.00%	0.18	85.91	2.63	1263.04	6.96%
1.3	0.22	99.55	103.05%	0.18	83.15	2.90	1329.54	6.58%

Table 6 - Average Normalized Yields and Purities With Varying NaCl

NaCl Normality	Average Yield	Average Purity
0.0	77.67%	7.76%
0.5	90.87%	6.82%
0.7	92.58%	6.11%
1.0	100.00%	6.89%
1.3	99.80%	6.40%
2.0	98.87%	6.54%

5 While NaCl normalities of 0.5 N and above were seen to give high yields, a normality of 1.0 N was selected as maximizing both yield and purity.

Table 7 - Formic Acid Optimization Data

Formic acid conc.	PI2 Area	Impurity Peak Area	Time (min)	Doublet Area	Time (min)	"Kunitz" Area	Time (min)
0.0%	7483.6	2453.50	15.63	6848.6	17.56	225054.1	~23.75 - 31.0
1.5%	7768.5	797.67	15.73	6008.5	17.54	138907.2	~23.75 - 29.25
0.1%	8252.0	2867.90	15.59	7071.5	17.54	226680.4	~23.75 - 30.5
0.5%	7165.9	2071.70	15.65	6198.6	17.53	203839.7	~23.75 - 30.5
1.0%	8353.7	813.80	15.61	5873.0	17.50	161433.2	~23.75 - 29.25
1.5%	7939.3	893.50	15.64	5979.0	17.54	135420.3	~23.75 - 29.25
0.1%	7005.0	1805.90	14.85	7788.5	17.00	233105.7	~23.25 - 30.0
1.5%	7407.2	962.20	15.10	6109.7	16.98	144764.2	~23.5 - 29.0
2.0%	7116.2	1117.55	15.11	6441.2	16.97	187670.8	~23.25 - 30.0
2.5%	7318.8	1176.40	15.07	6649.6	16.97	180476.2	~ 23.25 - 30.0

Table 8 - Formic Acid Optimization Data

Formic acid conc.	PI2 Area	PI2 (mg/ml)	Impurity Peak Area	Protein (mg/ml)	Doublet Area	Protein (mg/ml)	"Kunitz" Area	Protein (mg/ml)
0.0%	7483.6	0.19	2453.50	0.09	6848.6	0.17	225054.1	4.37
1.5%	7768.5	0.23	797.67	0.09	6008.5	0.19	138907.2	2.82
0.1%	8252.0	0.20	2867.90	0.10	7071.5	0.18	226680.4	4.40
0.5%	7165.9	0.18	2071.70	0.08	6198.6	0.16	203839.7	3.96
1.0%	8353.7	0.20	813.80	0.06	5873.0	0.16	161433.2	3.15
1.5%	7939.3	0.19	893.50	0.06	5979.0	0.16	135420.3	2.65
0.1%	7005.0	0.18	1805.90	0.08	7788.5	0.19	233105.7	4.53
1.5%	7407.2	0.18	962.20	0.06	6109.7	0.16	144764.2	2.83
2.0%	7116.2	0.18	1117.55	0.06	6441.2	0.17	187670.8	3.65
2.5%	7318.8	0.18	1176.40	0.06	6649.6	0.17	180476.2	3.52

Table 9 - Formic Acid Optimization Data

Formic acid conc.	PI2 (mg/ml)	PI2 mg	Imp. (mg/ml)	Impurity mg	Doublet (mg/ml)	Doublet mg	"Kunitz" (mg/ml)	"Kunitz" mg	Yield	Purity
0.0%	0.19	88.80	0.09	42.64	0.17	82.97	4.37	2085.22	79.93%	3.86%
1.5%	0.23	111.08	0.09	44.15	0.19	94.18	2.82	1370.31	100.00%	6.86%
0.1%	0.20	98.57	0.10	47.76	0.18	87.43	4.40	2159.78	104.57%	4.12%
0.5%	0.18	85.43	0.08	38.93	0.16	76.60	3.96	1880.60	90.63%	4.10%
1.0%	0.20	94.56	0.06	28.10	0.16	75.38	3.15	1529.05	100.56%	5.69%
1.5%	0.19	94.26	0.06	28.71	0.16	76.02	2.65	1280.14	100.00%	6.37%
0.1%	0.18	88.79	0.08	38.60	0.19	96.35	4.53	2271.21	96.55%	3.56%
1.5%	0.18	91.96	0.06	30.23	0.16	79.53	2.83	1407.70	100.00%	5.71%
2.0%	0.18	88.75	0.06	31.56	0.17	82.31	3.65	1809.93	96.50%	4.41%
2.5%	0.18	88.56	0.06	31.37	0.17	82.33	3.52	1700.64	96.30%	4.65%

Table 10 - Average Normalized Yields and Purities With Varying Formic Acid

% Formic acid	Average yield	Average purity
0.0	79.93%	3.86%
0.1	100.56%	3.84%
0.5	90.63%	4.10%
1.0	100.56%	5.69%
1.5	100.00%	6.31%
2.0	96.50%	4.41%
2.5	96.30%	4.65%

The data indicate the use of 1.5% formic acid content for the extraction solution. While other formic acid concentrations offer similar yield, 1.5% formic acid content clearly maximizes purity.

### Example 3

An experiment was conducted to determine the effect on yield by using varying amounts of the extraction solution comprised of 1.5% formic acid and 1.0 N NaCl in water. The weight ratio of potatoes to extraction solution was varied from 1:1 to 1:10. The ratios used and the observed yields are reported in Table 11.

Table 11 - Average Normalized PI2 Yield and Liquid Yield With Varying Extraction Ratio

Extraction ratio	Normalized, Average Yield	Average Yield in mg/kg
0.1	22.38%	24.07
0.2	60.47%	64.94
0.3	85.56%	91.98
0.4	100.00%	107.32
0.5	100.42%	107.76
0.6	101.03%	108.49
0.7	100.42%	107.74
0.8	100.74%	108.09
0.9	101.21%	108.57
1.0	101.38%	108.81

While the highest yield is achieved with the highest ratio of extraction solution, the gain in total yield is minimal above the 0.4 to one ratio (1:2.5 w/w extraction solution to potatoes, respectively). This ratio has been selected, in order to minimize extraction solution cost and material handling concerns, such as heating, cooling and evaporation.

The data dictate the choice of approximately 1.0 N sodium chloride as the preferred concentration in the extraction solution for the isolation of PI2. Using 1.0 N sodium chloride results in maximized yield of PI2 under the tested conditions, and although other concentrations are capable of producing similar yields, the PI2 protein purity that is represented by the use of 1.0 N NaCl is maximized at 1.0 N. Higher PI2 protein purity could be achieved by using less sodium chloride, however this would result in a reduced PI2 yield. This level of sodium chloride is also appropriate for the removal of the Kunitz type impurities. Similarly, the data dictate the selection of 1.5% formic acid as the preferred concentration for the extraction of PI2. An extraction solution that contains 1.5% formic acid exhibits beneficial antimicrobial and anti-proteolytic behavior. The yield of PI2 is maximized under the tested conditions at 1.5% formic acid content in the extraction solution, and this concentration also provides the highest PI2/Kunitz purity of the formulations that attain comparable yields. There is no significant increase in total yield when creating a slurry that is composed of greater than thirty percent extraction solution by weight. A slurry of thirty percent extraction solution composition is roughly equivalent to a one-part extraction solution to two and one-half parts raw material (1:2.5 solvent:solid ratio).

#### Example 4

A liquid extraction solution containing approximately 1.0 N sodium chloride and 1.5% formic acid was found to be effective in solubilizing PI2 while retaining its functional stability. The extraction system was examined to optimize the release of the target protein from the potato cellular matrix. Physical grinding is necessary to rupture the potato tuber cells and thereby release the protein into the liquid phase. The final grind profile of the potato slurry was examined for complete release of soluble proteins into liquid phase, minimal PI2 degradation, and ease of liquid/solid separation. Grind profile and extraction efficiency correlations were examined, followed by separation ease of the optimized grind profile.

A set of stackable sieves conforming to ASTM specification 11 is assembled with the largest sieve size on top and the rest placed in descending sieve size. The sieve size range should be chosen so as to capture at least 95 % of the solids in the suspension to be sized. Approximately 250 grams of the suspension to be sized is poured onto the top of the sieve stack. The top sieve is washed repeatedly with water until no more solids appear to be passing through the sieve. This sieve is then removed and this washing repeated for each sieve. The contents of each sieve are placed in pre-weighed weigh boats and placed in a vacuum oven at less than 100° C, but more than 50° C, to dry for at least 12 hours. After the solids are dry their weights are measured on an analytical balance and recorded. The particle size distribution is reported as the dry weight of the solids retained on each sieve expressed as a percentage of total dry solids retained. Results are reported in Table 12 using micrometers as the size unit.

Table 12 - Sample Size Distribution Report

Particle Size $\mu$ (micrometers)	% Solids Retained
1170	11
1080	32
625	38
400	19

For these trials whole, raw potatoes were extracted using an aqueous solution of 1.5 % formic acid and 1.0 N NaCl in a weight ratio of 1:2.5 extraction solution to potatoes. PI2 concentration was derived using reverse phase HPLC method described previously.

The degree of disintegration of the potato in the presence of the extraction solution has been studied. To test this aspect of the extraction, samples of the optimized extraction solution and whole, raw potatoes were ground using commercially available Commitrol grinders. The test protocol was designed to determine the grinding device's ability to generate to a number of consistent target profiles, and examine the particle size distribution within these grinds. The experimentally ground slurries were analyzed for PI2 content. A trend was discovered in which a finer grind profile exhibited increased yield of PI2 on a mg/kg basis. Extractions with an average particle size of greater than 1000  $\mu\text{m}$  showed a marked diminution of PI2 extraction efficacy.

When ground on a Urschel grinder to a nominal particle size of less than 100  $\mu\text{m}$ , the samples yielded 85 mg PI2 per kg of potato. A similar test done using the same lot of potatoes and extractive solution using a Hobart grinder giving a grind size of approximately 1500  $\mu\text{m}$  afforded 70 mg PI2 per kg of potato.

Table 13 - Comparison of Coarse and Fine Grind Processes

Grinder	Potatoes (kg)	Extraction solution	Average particle size- $\mu\text{m}$ (micrometers)	Total slurry (kg)	PI2 mg/kg potato
Hobart Coarse	5.59	2.24	~1500	7.83	70
Urschel Fine	5.72	2.29	<90	11.03	85

There was not an appreciable difference of ease of filtration under the conditions adopted for this experiment. The final pulp recovered from the Urschel grind was 17.3% by weight of the slurry and contained a moisture level of 49.8%. The pulp recovered from the Hobart grind was 31.9% by weight of the slurry and contained a moisture level of 60.5 %. This represents a potential loss in yield of approximately 10 percent in the more coarse grind profile, using a liquid yield weight percentage (7.1% residual liquid in the finely ground waste solids as opposed to 17.2% residual liquid in the coarsely ground waste solids).

In addition to PI2 and mass balance losses, the finer grind does exhibit a greater amount of total protein extracted using the finer grind protocol. The resulting liquid extracts were assayed using the reverse phase HPLC method. The fine grind extract does contain a greater

concentration of undesirable proteins. In particular, the PI2/Kunitz purity (taken as the concentration of PI2 divided by the total concentration of the Kunitz impurities and the PI2) decreases from 7.41 percent purity for the coarse grind and 5.99 percent purity in the extract resulting from the fine grind.

5 A further study examined the yield of PI2 using a variety of grind profiles. The grind profiles examined varied from 300  $\mu\text{m}$  average particle size to 1200  $\mu\text{m}$  average particle size.

Table 14 - Optimization of Grinding Profile and PI2 Yield

Average grind profile	Gap	PI2 yield	Kunitz content	PI2/'Kunitz' purity	Temperature increase
Approx. 300 micron	214 $\mu$	98.55%	105.77%	48.23%	13.1° C
Approx. 500 micron	388 $\mu$	100.00%	100.00%	50.00%	10.4° C
Approx. 700 micron	633 $\mu$	93.68%	97.94%	48.89%	8.8° C
Approx. 900 micron	968 $\mu$	91.32%	94.88%	49.05%	6.7° C
Approx. 1200 micron	1519 $\mu$	86.57%	84.97%	50.47%	5.2° C

Table 14 presents the optimization study for final grind profile with respect to PI2 yield. The yields and purities are normalized to the highest PI2 yield in the sample set. The highest yield was observed at approximately 500  $\mu\text{m}$  average particle size. The PI2/Kunitz purity is also acceptable, only one other grind profile exhibited a higher purity, however with an unacceptable sacrifice in PI2 yield. In order to produce the desired grind profile at the pilot scale, a "Microcut Head Assembly" was used. The final grind profile is determined by several mechanical characteristics of the grinding head, such as the number, spacing and angle of blades in the head as well as the speed and type of impeller. The Microcut head features 190 tungsten carbide blades, each .084 inches thick. This thickness allows for a spacing of .0153 inches (388.62  $\mu$ ) between each blade. The product is pushed through the spaces between the blades by the impeller. The impeller being used is a "veri-cut" due to its durability and the uniform particle size it produces. This impeller, in conjunction with this head assembly, produces a depth of cut of .0016 inches (40.64  $\mu$ ). The interaction of the impeller, grinding blades and raw materials generates the friction responsible for the observed temperature rise. A rise of ten degrees was not considered harmful, due to the heat stability of PI2 (70° C for <sup>more</sup> ~~ore~~ than 3 hours). The depth of cut may vary slightly with the speed of the impeller, which is determined by the motor. For

these studies, a consistent grind profile was used to provide an average particle size of approximately 500  $\mu$ .

Trials were then conducted, using the optimized grind profile, to determine the proper separation conditions of the liquid/solid slurry. There are many techniques available to separate solids from liquids. A basket type centrifuge was identified as appropriate for the separation of potato solids from the extraction solution mixture. The target goals for the separation process were to maximize the liquid extracted from the slurry, while generating a cake with a minimized moisture content. As the PI2 is expected to disperse within the liquid fraction, maximizing liquid recovery is of primary importance to maximizing the yield of PI2. Pilot trials were performed, using a pilot model that would be directly scaleable to a full production model. The characteristic of the centrifuge that was optimized by these trials was the filter-mesh screen size.

Table 15 - Screen Mesh Trial for Optimization

Mesh size	Liquid recovery	Solid moisture content	Suspended solid	Time per L collected
100 $\mu$	100.00%	5.35%	5.35%	0.972 L/min
75 $\mu$	99.87%	5.78%	4.55%	0.968 L/min
50 $\mu$	99.54%	5.94%	1.05%	0.967 L/min
35 $\mu$	99.13%	6.05%	0.25%	0.960 L/min
15 $\mu$	98.65%	6.74%	0.15%	0.933 L/min

The liquid recovery data was normalized to the highest yield examined over the data set, the moisture content if the solid cake was measured via vacuum oven digestion, and the suspended solids were determined via gyro-testing. Based on the data from Table 15, a 35 $\mu$  filter bag mesh was chosen for continued pilot study, and for full production. The liquid yield is maximized (over the sample set tested) utilizing the largest screen mesh. Unfortunately, this screen mesh also generates the highest amount of suspended solid in the filtered extract. It can be observed that a dramatic reduction in the amount of suspended solid is observed using filter bags below 75 $\mu$ . The reduction of suspended solids achieved using a 35 $\mu$  filter, combined with the acceptable yield and collection rate, made the 35 $\mu$  bag the preferred choice.

The foregoing description comprise illustrative embodiments of the present inventions. The foregoing embodiments and the methods described herein may vary based on the ability, experience, and preference of those skilled in the art. Merely listing the steps of the method in a



